



USING FUZZY LOGIC TO CONTROL ACTIVE SUSPENSION SYSTEM OF ONE-QUARTER-CAR MODEL

Ramtin Rakhsha ^{*1}, Seyed assadollah Ghazavi², Naser Yasrebi³

School of mechanical engineering, University of Tehran, Tehran, IRAN
(E-mail: Ramtin_Rakhsha@yahoo.com)

Abstract

In this paper, fuzzy logic is used to control active suspension of one-quarter car model. The main role of a car suspension system is to improve the ride comfort and to better the handling property. It usually consists of a spring and a damper to improve the properties of suspension system. The fuzzy logic method is one of the most active research and developments areas on artificial and intelligence now, particularly in the automobile industry. One quarter of car is modeled by springs, masses, dampers, force actuator, and the state space equations are derived by lagrangian method. The ride comfort is improved by means of the reduction of the body acceleration caused by the car body when road disturbance from uneven road surfaces, pavement point etc. act on the tires of running car. Here, a logic fuzzy controller is designed in which, the number of rule bases are reduced in comparison with some traditional one that have been introduced in other papers. At the end, a comparison of active suspension fuzzy control and traditional passive suspension is shown using MATLAB simulations. Results show that, active suspension improves the ride comfort by reducing acceleration, compared with the performance of passive suspension.

INTRODUCTION

Replacement of the spring-damper suspension of automobiles by active systems has been the potential of improving safety and comfort under nominal conditions. Research and development of active suspension systems for car models are increasing much in recent years, because the active suspension systems offer good riding comfort to passengers [1]. For the design of the active suspension, we know how to build a model and how to define the objective of the control in order to reach a compromise between contradictory requirements like ride comfort and road holding by changing the force between the wheel and body [2]. Body acceleration is the most important element in the ride comfort. By reducing the acceleration of the car body, we can get more comfort in riding.

The core of this work is to evaluate benefits of fuzzy controller under impulse input for road velocity. There are taken the velocity of the body and deflection

velocity between body and wheel, as input data for fuzzy controller and active force as its output data. The objective of the control is to minimize the body acceleration and displacement when road disturbances are acting on the tires of running cars.

ONE-QUARTER-CAR MODEL

In this paper, we are considering a one-quarter-car model include body mass, wheel mass, two springs, one damper and one force actuator (HYNIOVÁ, STRÍBRSKÝ and HONCŮ, 2001, [3]). See Figure.1.

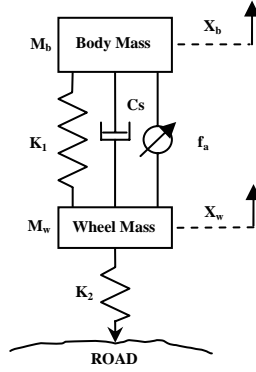


Figure 1 - One-quarter-car model (2 degree of freedom)

This model is used to create control force between body and wheel. The model has two degree of freedom: \mathbf{X}_b and \mathbf{X}_w .

Using Lagrangian method:

$$\frac{d}{dt} \frac{\partial(K.E.)}{\partial \dot{q}_i} - \frac{\partial(K.E.)}{\partial q_i} + \frac{\partial(P.E.)}{\partial q_i} + \frac{\partial(D.E.)}{\partial \dot{q}_i} = 0 \quad (1)$$

Where:

$$\begin{aligned} K.E. &= \frac{1}{2} m_b (\dot{x}_b)^2 + \frac{1}{2} m_w (\dot{x}_w)^2 \\ P.E. &= \frac{1}{2} K_1 (x_b - x_w)^2 + \frac{1}{2} K_2 (x_w - x_r)^2 \\ D.E. &= \frac{1}{2} C_s (\dot{x}_b - \dot{x}_w)^2 - f_a (\dot{x}_b - \dot{x}_w) \end{aligned} \quad (2)$$

If $i=1$, for $q_1=x_b$

$$m_b \ddot{x}_b + K_1 (x_b - x_w) + C_s (\dot{x}_b - \dot{x}_w) - f_a = 0 \quad (3)$$

and if $i=2$, for $q_2=x_w$

$$m_w \ddot{x}_w - K_1 (x_b - x_w) + K_2 (x_w - x_r) - C_s (\dot{x}_b - \dot{x}_w) + f_a = 0 \quad (4)$$

with the following constants and variables which respect the static equilibrium position:

\mathbf{x}_b :	Body displacement	\mathbf{m}_b :	Body mass (one-quarter of the total body mass of the car)= 250 Kg
\mathbf{x}_w :	Wheel displacement	\mathbf{m}_w :	Wheel mass= 35 Kg
\mathbf{x}_r :	Road displacement	\mathbf{K}_1 :	Stiffness of the body= 16000 N/m
\mathbf{f}_a :	Desired force	\mathbf{K}_2 :	Stiffness of the wheel= 160000 N/m
\mathbf{C}_s :	Damping ration of the damper = 980 Ns/m		

State-Space model

To model the road input, let us assume that the vehicle is moving with a constant forward speed. Then the vertical velocity can be taken as a white noise process that is approximately true for most of real roadways [1].

To transform the motion equations of one-quarter-car model into a state space model, the following state variables are considered:

$$\begin{aligned}
 x_1 &= x_b - x_w \dots\dots\dots \text{Body displacement} \\
 x_2 &= x_w - x_r \dots\dots\dots \text{Wheel displacement} \\
 x_3 &= \dot{x}_b \dots\dots\dots \text{Absolute velocity of the body} \\
 x_4 &= \dot{x}_w \dots\dots\dots \text{Absolute velocity of the wheel}
 \end{aligned}$$

Using Eq.3 and Eq.4:

$$\dot{x}_3 = \frac{1}{m_b} (-K_1(x_b - x_w) - C_s(\dot{x}_b - \dot{x}_w) + f_a) \quad (5)$$

$$\dot{x}_4 = \frac{1}{m_w} (K_1(x_b - x_w) - K_2(x_w - x_r) + C_s(\dot{x}_b - \dot{x}_w) - f_a) \quad (6)$$

These equations can be written in state space form as follows:

$$\dot{\mathbf{x}} = \mathbf{A}.\mathbf{x} + \mathbf{B}.f_a + \mathbf{L}.v_r$$

where:

$$\mathbf{A} = \begin{bmatrix} 0 & 0 & 1 & -1 \\ 0 & 0 & 0 & 1 \\ \frac{-K_1}{m_b} & 0 & \frac{-C_s}{m_b} & \frac{C_s}{m_b} \\ \frac{K_1}{m_w} & \frac{-K_2}{m_w} & \frac{C_s}{m_w} & \frac{-C_s}{m_w} \end{bmatrix} \quad \mathbf{B} = \begin{bmatrix} 0 \\ 0 \\ 1/m_b \\ -1/m_w \end{bmatrix} \quad \mathbf{L} = \begin{bmatrix} 0 \\ -1 \\ 0 \\ 0 \end{bmatrix}$$

by considering the state space as:

$$\begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

we have:

$$B = \begin{bmatrix} 0 & 0 \\ 0 & -1 \\ 1/m_b & 0 \\ -1/m_w & 0 \end{bmatrix} \quad u = \begin{bmatrix} f_a \\ \dot{x}_r \end{bmatrix} \quad C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 1 & -1 \end{bmatrix} \quad D = 0$$

The form of C is arbitrary; depending on the necessary data that should be appear in output of state space equations. There are three outputs for state space as bellow:

$$y = \begin{bmatrix} y_1 \\ y_2 \\ y_3 \end{bmatrix} = \begin{bmatrix} \text{Body displacement : } (x_b - x_w) \\ \text{Body velocity : } (\dot{x}_b) \\ \text{Deflection velocity : } (\dot{x}_b - \dot{x}_w) \end{bmatrix}$$

FUZZY LOGIC CONTROLLER

The fuzzy logic controller is used in this active suspension system. The control system itself consists of three stages: fuzzification, fuzzy inference engine and defuzzification [4]. See Figure 2.

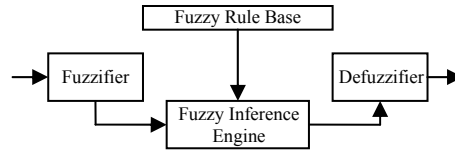


Figure 2 - Fuzzy function

The fuzzification stage converts real-number (Crisp) input values in to fuzzy values while the fuzzy inference machine processes the input data and computes the controller outputs in cope with the rule base and database. These outputs that are fuzzy values are converted in to real numbers by the defuzzification stage [2].

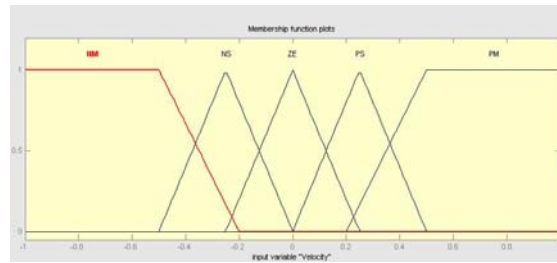


Figure 3 - Membership function for body velocity

The fuzzy logic controller has two inputs; absolute velocity of the body and deflection velocity and one output; desired force. The number of input data of the fuzzy controller is reduced from three to two in comparison with the model in ref.3. A possible choice of membership function for active suspension system represented by a fuzzy set is as clear:

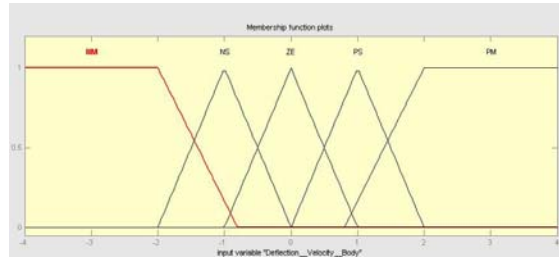


Figure 4 - Membership function for deflection velocity

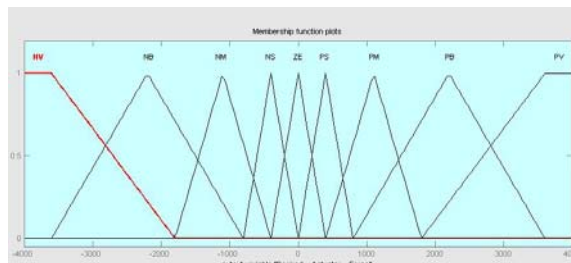


Figure 5 - Membership function for desired actuator force

One-quarter-car is modelled in ADAMS/view to get better rules by means of exact data. See Figure.6. The number of rule base of the fuzzy controller is reduced from 75 to 25 in comparison with some traditional one. See ref.3. The rule base used in the active suspension system for one-quarter-car model is represented by 25 rules with fuzzy terms derived by modelling the designer's knowledge and experience and ADAMS's data.

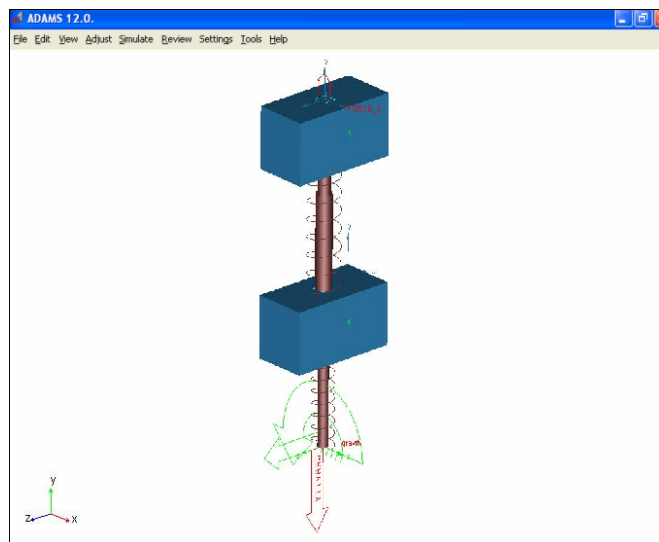


Figure 6 - One-quarter-car model in ADAMS/view

The abbreviations used correspond to:

NV	...	Negative very big	PV	...	Positive very big
NB	...	Negative big	PB	...	Positive big
NM	...	Negative medium	PM	...	Positive medium
NS	...	Negative small	PS	...	Positive small
ZE	...	Zero			

8. If (Deflection_Velocity_Body is ZE) and (Velocity is PS) then (Desired_Actuator_Force is NS) (1)
 9. If (Deflection_Velocity_Body is NS) and (Velocity is PS) then (Desired_Actuator_Force is NM) (1)
 10. If (Deflection_Velocity_Body is NM) and (Velocity is PS) then (Desired_Actuator_Force is NM) (1)
 11. If (Deflection_Velocity_Body is PM) and (Velocity is ZE) then (Desired_Actuator_Force is PS) (1)
 12. If (Deflection_Velocity_Body is PS) and (Velocity is ZE) then (Desired_Actuator_Force is ZE) (1)
 13. If (Deflection_Velocity_Body is ZE) and (Velocity is ZE) then (Desired_Actuator_Force is ZE) (1)
 14. If (Deflection_Velocity_Body is NS) and (Velocity is ZE) then (Desired_Actuator_Force is ZE) (1)
 15. If (Deflection_Velocity_Body is NM) and (Velocity is ZE) then (Desired_Actuator_Force is NS) (1)
 16. If (Deflection_Velocity_Body is PM) and (Velocity is NS) then (Desired_Actuator_Force is PM) (1)
 17. If (Deflection_Velocity_Body is PS) and (Velocity is NS) then (Desired_Actuator_Force is PM) (1)
 18. If (Deflection_Velocity_Body is ZE) and (Velocity is NS) then (Desired_Actuator_Force is PS) (1)

Figure 7 - Schematic rule base

The following table represents the rule base:

Table 1 - Rule base

	$\dot{x}_b - \dot{x}_w$	\dot{x}_b	f_a		$\dot{x}_b - \dot{x}_w$	\dot{x}_b	f_a		$\dot{x}_b - \dot{x}_w$	\dot{x}_b	f_a
1	PM	PM	ZE	9	NS	PS	NM	17	PS	NS	PM
2	PS	PM	NS	10	NM	PS	NM	18	ZE	NS	PS
3	ZE	PM	NM	11	PM	ZE	PS	19	NS	NS	PS
4	NS	PM	NM	12	PS	ZE	ZE	20	NM	NS	ZE
5	NM	PM	NB	13	ZE	ZE	ZE	21	PM	NM	PB
6	PM	PS	ZE	14	NS	ZE	ZE	22	PS	NM	PM
7	PS	PS	NS	15	NM	ZE	NS	23	ZE	NM	PM
8	ZE	PS	NS	16	PM	NS	PM	24	NS	NM	PS
				25	NM	NM	ZE				

The rules of the controller have the general form of:

$$Rule_i: \text{IF } (\dot{x}_b - \dot{x}_w = P_i) \text{ AND } (\dot{x}_b = Q_i) \text{ THEN } (f_a = R_i)$$

where P_i , Q_i and R_i are labels of fuzzy sets representing the linguistic values of $\dot{x}_b - \dot{x}_w$, \dot{x}_b and f_a , respectively which are characterized by their membership functions.

The output of the fuzzy controller is in fuzzy set, thus, the method that is used for diffuzzification is "Centre of Gravity Method".

SIMULATION RESULTS

In this section, the controller was tested and analyses have been developed to compare the results of active suspension system with a traditional passive one. The pulse response of the model is shown in Figure 8. The input of the controller is road

velocity. We consider the pulse as its input with magnitude of 10. It is equal to the step with 10cm height as road displacement.

As shown in Figure 8, the magnitude of the acceleration decreased to some extent by using fuzzy controller that improves the ride comfort index. The solid curve is related to the active suspension system and the dashed one is for traditional model.

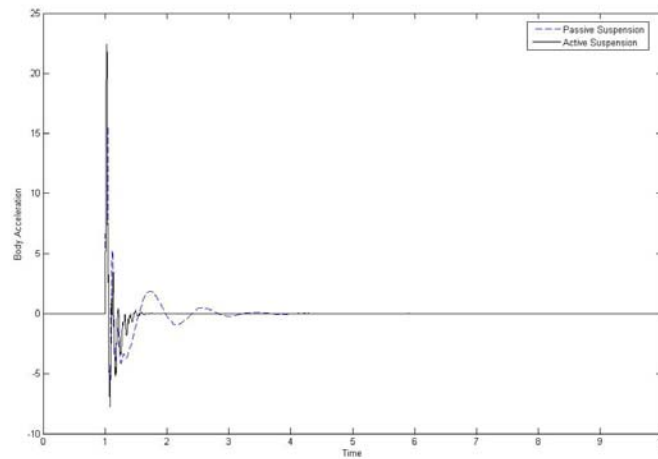


Figure 8 - Variations of acceleration magnitude vs. time

It is clear that the acceleration has been damped less than 0.5 seconds. The fuzzy command is shown in Figure 9.

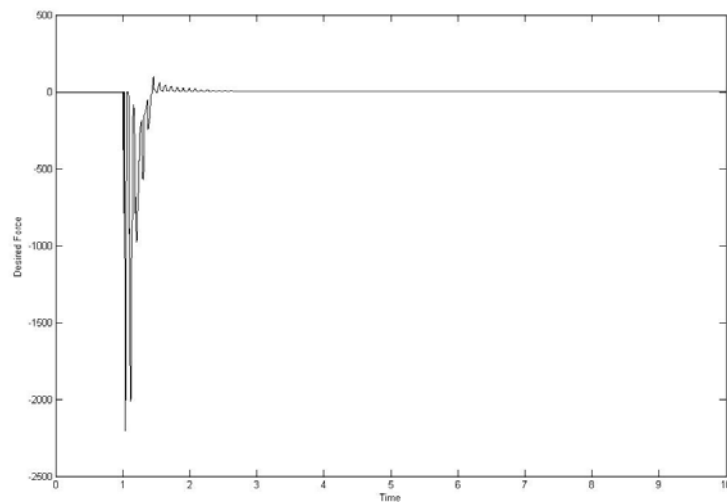


Figure 9 - Fuzzy command vs. time

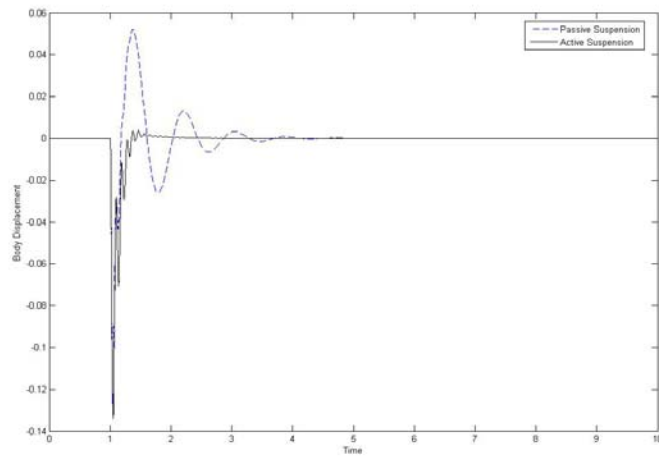


Figure 10 - Body displacement vs. time

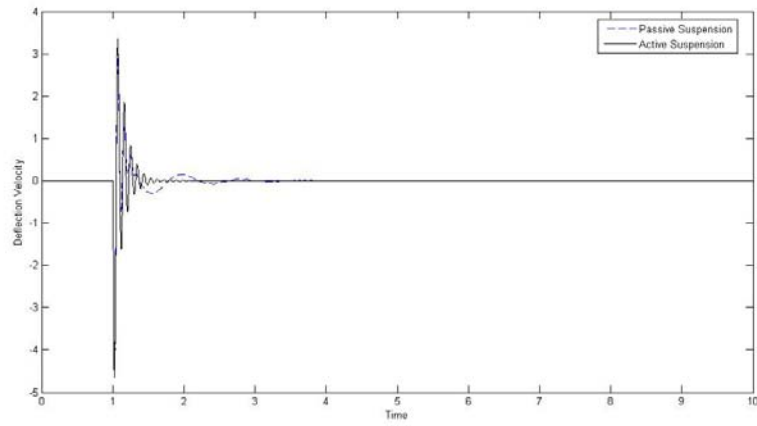


Figure 11 - Deflection velocity vs. time

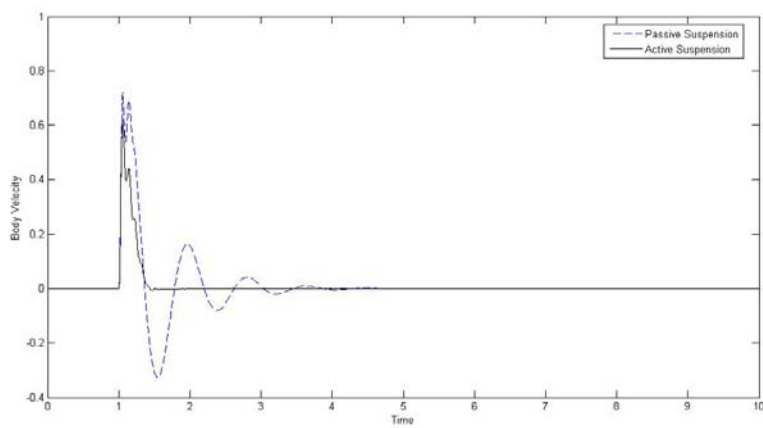


Figure 12 - Body velocity vs. time

CONCLUSIONS

By replacing the traditional model by active suspension, we can control and reduce the displacement and acceleration to achieve ride comfort. The effects of active suspension on acceleration have been investigated. Results show that active suspension improves the ride comfort by reducing acceleration compared with the performance of the passive one.

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