# ANALYSIS AND OPTIMIZATION OF APERTURE DESIGN IN COMPUTATIONAL IMAGING

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#### ABSTRACT

There is growing interest in the use of coded aperture imaging systems for a variety of applications. Using an analysis framework based on mutual information, we examine the fundamental limits of such systems—and the associated optimum aperture coding—under simple but meaningful propagation and sensor models. Among other results, we show that when SNR is high and thermal noise dominates shot noise, spectrally-flat masks, which have 50% transmissivity, are optimal, but that when shot noise dominates thermal noise, randomly generated masks with lower transmissivity offer greater performance. We also provide comparisons to classical pinhole and lens-based cameras.

*Index Terms*— coded aperture cameras, computational photography, optical signal processing

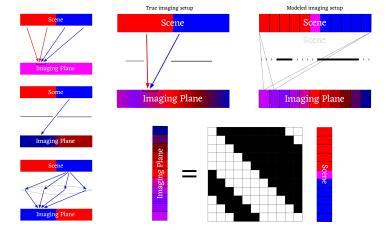
## 1. INTRODUCTION

Digital signal processing plays an important role in modern imaging systems. Many modern imaging systems operating at optical and higher frequencies use coded apertures, whereby the traditional lens in the aperture is replaced with a spatial mask that selectively blocks portions of the light from reaching the sensor. Yet while this is an increasingly important imaging modality—and one with a long history dating back to the earliest pinhole cameras—typical mask designs are guided by heuristics and/or numerical procedures.

As Figure 1 depicts, with an empty aperture, scene recovery from measurements at the imaging plane is very poorly conditioned. Coded-aperture cameras seek to improve the conditioning of the problem through the use of more complicated (and transmissive) masks than a pinhole, in combination with suitably designed post-processing.

In this paper, we develop a comparative analysis of these imaging systems, using mutual information as our performance measure. We use far-field geometric optics to model propagation, and our sensor model at the imaging plane includes thermal and shot noise components.

Among the earliest and simplest instances of codedaperture imaging are those based on pinhole structure [1, 2] and pinspeck (anti-pinhole) structure [3], though more complex structure is often used. Other methods involve cameras that uses a mask in addition to a lens to, e.g., facilitate depth estimation [4], deblur out-of-focus elements in an image [5], enable motion deblurring [6], and/or recover 4D lightfields



**Fig. 1**: Three imaging systems (left, top-to-bottom): no aperture, a pinhole and a lens. Arrows indicate paths light from the scene takes to a particular point on the imaging plane. On the right is an arbitrary mask, an illustration of its discretization and the corresponding transfer matrix.

[7]. Some forgo the lens altogether to decrease costs and/or meet physical constraints [8] [9].

Certain other systems, intended for non-line-of-sight applications, rely on known structure in between the scene and the imaging plane to improve the conditioning of the problem [10, 11, 12]. These can be viewed as instances of the broader class of coded-aperture systems that we analyze, in which the mask is naturally occuring and not chosen.

# 2. MODEL

Scene. Let I(x) [W/m] represent the intensity of the scene over space in one dimension:  $0 \le x \le L$ . We denote  $J = \int I(x) \mathrm{d}x$  [W] the net power radiated. Assume a uniform discretization of [0,L] into n bins of size  $\Delta = L/n$  each, and denote  $x_1, x_2, \ldots, x_n$  their centers. We assume that the discretization is fine enough that the intensity at each bin  $i \in [1,n]$  takes constant value  $I(x_i)$ . Let  $f_i = I(x_i) \cdot \Delta$  be the power radiated from each bin. We model  $\mathbf{f} = [f_1, \ldots, f_n]$  as a multivariate Gaussian distribution  $\mathcal{N}(\mu \mathbf{1}, \mathbf{Q})$  with mean  $\mu$  and covariance matrix  $\mathbf{Q}$ . We set  $\mu = J/n$  to ensure that the average net power is the expectation of the sum of the power radiated from each bin  $\mathbb{E}[\sum_{i \in [1,n]} f_i] = \sum_{i \in [1,n]} \mu = J$ . The Gaussian statistics model for images is frequently used,

such as in [13, 4]. In this paper, we consider the following two cases:

IID: We assume that the  $f_i$ 's are uncorrelated, i.e.,  $\mathbf{Q} = \frac{\theta}{n}\mathbf{I}$ . While natural scenes will exhibit correlations, studying the IID case is a means of performing a worst-case analysis. The scaling by 1/n ensures that the variance of the total scene intensity  $\sum_i f_i$  is independent of n;  $\theta>0$  is a parameter that captures the variance in total intensity between different scenes. To ensure non-negativity of the  $f_i$ 's, let  $J>>\sqrt{\theta}$ . Decaying-frequency prior: We follow a simple statistical model according to which the power spectrum of natural image decays exponentially with the spatial frequency [14] by taking  $\mathbf{Q} = \mathbf{F}_n^* \mathbf{D}^* \mathbf{F}_n$ , where  $\mathbf{F}_n$  is the normalized DFT matrix of size n and  $\mathbf{D}^*$  is a diagonal matrix with the following entries:  $d_1 = 1$ ,  $d_i^* = d_{n-i+1}^* = \frac{\theta}{n} \beta^{\frac{i-1}{(n-1)/2}}$ ,  $i = 2, \ldots, \lceil (n+1)/2 \rceil$ , for some frequency decay rate parameter  $0 < \beta < 1$ . A lower  $\beta$  implies a more strongly correlated

**Aperture**. Denote by  $\widetilde{\mathbf{A}}$  an  $n \times n$  transfer matrix whose entries  $\widetilde{\mathbf{A}}_{ji}$  model the aperture. Because the aperture cannot create light, only redirect or absorb it, we have that the column-sums of  $\widetilde{\mathbf{A}}$  are at most 1, i.e.  $\sum_j \widetilde{\mathbf{A}}_{ji} \leq 1$ . We assume that a maximal integration time is allowed, and for convenience we normalize it,  $\mathbf{A} = n\widetilde{\mathbf{A}}$ , so that the normalized transfer matrices  $\mathbf{A}$  for absorbing (non-redirecting) apertures are  $\{0,1\}$  matrices. Denote by  $\rho$  the *transmissivity* of the aperture. For an on-off aperture,  $\rho$  measures the fraction of elements that transmit light (See Fig. 1). In general, we assume a circulant  $\mathbf{A}$ ; that is equivalent to assuming that the mask repeats a certain pattern (of length n) twice:  $\mathbf{A}_{ji} = a_{(i-j) \mod n}$  where  $\mathbf{a}^T = (a_0, \dots, a_{n-1})^T$  is the first row of  $\mathbf{A}$ .

Imaging plane. The imaging plane consists of n adjacent and equally-sized pixels. The power  $y_j$  measured at each pixel is  $y_j = \frac{1}{n} \sum_{i=1}^n A_{ji} \cdot f_i$ , where  $f_i$  is the power radiated from the  $i^{\text{th}}$  bin. The (1/m)-scaling is chosen to ensure preservation of energy:  $\mathbb{E}[\sum_j y_j] = \frac{1}{n} \sum_j \sum_i A_{ji} \cdot \mathbb{E}[x_i] \leq \frac{1}{n} \cdot n^2 \cdot \frac{J}{n} = J$ . The measurement model is a reduction of a more complete forward model, which accounts for distance attenuation and cosine factors in light propagation [15]. This reduction corresponds to a scenario where the scene is far enough from the imaging plane that the distance attenuation and cosine factors are well-approximated by constants.

**Noise.** We distinguish between two different types of noise. (*Thermal noise*): This includes noise sources that are independent of the contribution to the measurements due to the scene of interest. We model it as additive Gaussian with variance W/n, where W denotes the constant net noise power and each pixel absorbs power proportional to its size, giving rise to the 1/n factor.

(Shot noise): This includes measurement noise that depends on the contribution due to the scene of interest. This results in additive Gaussian noise of variance  $\rho \cdot \frac{J}{n}$  (proportional to the net power of light that goes through the aperture).

Overall, the measurement at each pixel is modeled as  $y_i =$ 

 $\sum_{i \in [1,n]} \widetilde{\mathbf{A}}_{ji} f_i + z_j, \text{ where } z_j \sim \mathcal{N}(0, (W + \rho \cdot J)/n).$  **Mutual information**. The mutual information (MI) between the measurements  $y_j, j \in [n]$  and the unknowns  $f_i, i \in [1,n]$  of the imaging problem is given as  $\mathcal{I} = \log \det \left(\frac{1}{\sigma^2} \widetilde{\mathbf{A}} \mathbf{Q} \widetilde{\mathbf{A}}^T + \mathbf{I}\right)$ , where the noise variance  $\sigma^2 = (W + \rho \cdot J)/n$ . Recall that a circulant matrix is diagonalized by  $\mathbf{F}_n$ . Also,  $\mathbf{Q} = \mathbf{F}_n^* \mathbf{D} \mathbf{F}_n$  where  $\mathbf{D} = \frac{\theta}{n} \mathbf{I}$  (IID scene) or  $\mathbf{D} = \mathbf{D}^*$  (1/f-prior). With these,  $\mathcal{I}$  reduces to (recall  $\mathbf{A} = n \widetilde{\mathbf{A}}$ )

$$\mathcal{I} = \sum_{i=1}^{n} \log \left( \frac{1}{W + \rho \cdot J} \cdot d_i \cdot \frac{|\lambda_i(\mathbf{A})|^2}{n} + 1 \right), \quad (1)$$

where  $\lambda_i(\mathbf{A})$  denotes the eigenvalue of  $\mathbf{A}$  corresponding to the  $i^{\text{th}}$  frequency and  $d_i$  denotes the  $i^{\text{th}}$  entry on the diagonal of  $\mathbf{D}$ . We often write  $\lambda_i$  when clear from context.

**Aperture Types**. Here, we summarize several types of aperture designs and their corresponding models.

*Pinhole:* We model a pinhole camera as an on-off mask with only a single open element, i.e.,  $\mathbf{A} = \mathbf{I}$  (or, any permutation of the identity). This implies  $\rho = 1/n$ .

*Lens:* We model a lens assuming the scene lies entirely at the focal plane of the lens, in which case it behaves like a pinhole with much higher intensity:  $\widetilde{\mathbf{A}} = \mathbf{I}$  (see Fig. 1).

Spectrally-Flat patterns: The family includes pseudo-noise binary (0/1) patterns such as maximum length sequences (MLS) and uniform redundant array patterns such as URA and MURA. Onwards, we refer to patterns with the following properties as spectrally-flat patterns: (i)  $\rho \approx 1/2$  (there may be one more one than zero); (ii) they are spectrally flat with the exception of a DC term [16, 17, 18, 19].

Random on-off patterns: We study random patterns where each entry of **a** is generated IID  $\operatorname{Bern}(p)$ , for  $p \in (0,1]$ . For such random on-off patterns we use  $\rho = p$ , since for large n (which is our focus) the number of on-elements is  $\approx np$ .

Random uniform patterns: We also study patterns consisting of elements that can partially absorb light, e.g., [20, 7]. We focus on random such patterns where each entry of a is IID Uniform([0, 1]). For these patterns, the expected transmissivity  $\rho = 1/2$ .

# 3. RESULTS

# 3.1. IID scene

Throughout this section we study the IID scene model. It is convenient to define  $\gamma_{\rho}=\frac{\theta}{W+\rho J}$ , for  $0<\rho<1$ . We use  $\log(.)$  and  $\ln(.)$  to denote the base-2 and base-e logarithms, respectively. We express all values for the MI in bits.

# 3.1.1. Pinhole

From (1) the MI of a pinhole is given by  $\mathcal{I}_{pinhole} = n \log \left( \frac{\theta}{n(nW+J)} + 1 \right)$ . By allowing only a fraction of 1/n of the light to go through, the formula justifies that the performance of a pinhole deteriorates drastically for large n. Note that this result applies only to a vanishingly small pinhole (decreasing in size as n increases); a pinhole of fixed size achieves constant mutual information.

# 3.1.2. Lens

From (1) the *normalized* MI of a lens is given by  $\frac{1}{n}\overline{\mathcal{I}}_{\text{lens}} = \log(\frac{\theta}{W+J}+1)$ . Thus lenses outperform any purely absorbing (mask-based) aperture.

## 3.1.3. Spectrally-flat patterns

The following proposition characterizes the MI of spectrallyflat patterns and shows that they maximize MI when thermal noise is dominant. See Appendix A for a proof sketch.

**Proposition 3.1.** Consider the IID scene model. Let  $\mathcal{I}_{SF}$  be the mutual information of a spectrally-flat pattern for an odd n.<sup>1</sup> It holds that:

$$\lim_{n \to \infty} \mathcal{I}_{SF} = \log(\frac{\gamma_{1/2}}{4} + 1) + \frac{\gamma_{1/2}}{4\ln(2)}.$$
 (2)

Remark 1. For spectrally-flat occluders,  $\lambda_1 \approx \frac{n}{2}$  and  $|\lambda_2| = \ldots = |\lambda_n| \approx \frac{\sqrt{n}}{2}$ . Throughout, statements that involve  $n \to \infty$  are to be interpreted with the rest of parameters (such as  $W, J, \theta, \rho$ ) held constant (independent of n).

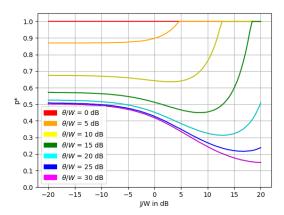
#### 3.1.4. Random on-off patterns

We explicitly compute the asymptotic value of the MI for random on-off patterns. Our theoretical results use tools from random matrix theory (RMT) [21, 22] and are thus asymptotic in nature. (However, numerical simulations suggest accuracy of the predictions for n on the order of a few hundreds.) A proof sketch is deferred to Appendix A.

**Proposition 3.2.** Assume the IID scene model. The mutual information  $\mathcal{I}_p$  for a random on-off circulant system with parameter  $0 converges in probability with <math>n \to \infty$  to:  $\widetilde{\mathcal{I}}_p = \log (p^2 \gamma_p + 1) + p(1 - p)\gamma_p / \ln(2)$ .

Remark 2. Maximizing  $\mathcal{I}_p$  over p gives the optimal choice  $p^\star$  of the transmissivity parameter. Given the formula of Prop. 3.2, it is possible to numerically evaluate  $p^\star$  for different values of the parameters  $J, W, \theta$ . See Fig. 2 for an illustration. Furthermore, by analyzing the derived asymptotic formula for the MI, it is possible to obtain analytic conclusions for some interesting regimes of parameters. For example, when thermal noise dominates  $(W >> \theta$  and W >> J), then using  $\log (p^2 \gamma + 1) \approx p^2 \gamma$  gives  $p^\star \approx 1$ ; i.e., an open aperture is optimal. When SNR is high and thermal noise is the stronger of the two noise sources  $(\theta >> W >> J)$ ,  $p^\star \approx 0.5$ ; when shot noise is stronger  $(\theta >> J >> W)$ ,  $p^\star$  is small.<sup>2</sup>

Remark 3. Comparing Prop. 3.1 to Prop. 3.2 reveals that in the  $n \to \infty$  limit, the performance of balanced random on-off circulant systems with p=1/2 approach the performance of spectrally-flat circulant systems.



**Fig. 2**: A plot of optimal transmissivity parameter  $p^*$  for random on-off patterns in the IID scene model, as we vary shot noise power J and signal strength  $\theta$  while ambient noise power W is held fixed. See Remark 2.

# 3.1.5. Random uniform patterns

Similarly to Proposition 3.2, we leverage results of [21] to evaluate the MI performance of random uniform patterns; we omit the details due to space limitations.

**Proposition 3.3.** Consider the IID scene model. The mutual information  $\mathcal{I}_{uniform}$  for a random uniform circulant system converges in probability with n to:  $\widetilde{\mathcal{I}}_{uniform} = \log(\frac{\gamma}{4} + 1) + \frac{\gamma}{12\ln(2)}$ , with  $\gamma = \frac{\theta}{W+J/2}$ .

Comparing the formula of the proposition to Proposition 3.2, reveals that  $\widetilde{\mathcal{I}}_{\text{uniform}} < \widetilde{\mathcal{I}}_p$ , for all  $p \in [\frac{1}{2}, \frac{1}{2} + \frac{1}{\sqrt{6}}]$ . Hence, random on-off masks in this range of p outperform random uniform masks. In short, if physical limitations prevent the use of apertures that can redirect light, but can only absorb it, then absorbing all or nothing (with appropriate p) is better than partial absorption (at least for random designs).

# 3.2. Correlated scene

We extend the "worst-case" analysis of the previous section regarding IID scenes to correlated ones. We follow the  $\beta^{-d}$  scene prior model. Due to space limitations, we restrict the exposition to spectrally-flat and random on-off patterns. For convenience, we assume n is odd.

Spectrally-flat patterns: For large enough n, we find that the MI of spectrally-flat patterns corresponds to:  $\lim_{n\to\infty} \mathcal{I}_{SF} = \log(\frac{\gamma_{1/2}}{4}+1) + \frac{\gamma_{1/2}(1-\beta)}{4\ln(2)\ln(1/\beta)}$ . The derivation of this result is a straightforward extension of (2), and we elide it for space.

Remark 4. In the  $\beta \to 1$  limit, correlations between the  $x_i$  approach 0, and it can be shown that the formula above approaches that in (2), as expected.

Random on-off patterns: Contrary to the case of IID scenes where knowledge of the the limiting spectral density of **A** suf-

<sup>&</sup>lt;sup>1</sup>Here, we implicitly assume that n is such that an MLS, or URA, or MURA pattern exists. For example, MURA patterns can be generated for any prime n that is of the form  $4d+1,\ d=1,2,\ldots$ 

<sup>&</sup>lt;sup>2</sup>Analyzing  $\frac{d\tilde{\mathcal{I}}_p}{dp}$  reveals that  $0 < p^* < \max\left(\sqrt{\frac{J}{\theta}}, \sqrt{\frac{W}{J}}\right)$ .

fices to characterize the MI, for correlated scenes each eigenvalue is weighted differently. Hence, the behavior of the MI depends on the statistics of each individual eigenvalue. Since **A** is circulant, the eigenvalues of A are exactly the Fourier coefficients of the entries of the generating vector **a**, i.e.,  $\lambda_1 = \sum_{\ell=0}^{n-1} a_\ell$ , and, for  $k=2,\ldots,\frac{n-1}{2}$  (assume n is odd for simplicity):  $\lambda_k^2 = \lambda_{n-k}^2 = g_k^2 + h_k^2$ , where  $g_k := \sum_{\ell=0}^{n-1} a_\ell \cdot \cos(\ell k \frac{2\pi}{n})$ ,  $h_k := \sum_{\ell=0}^{n-1} a_\ell \cdot \sin(\ell k \frac{2\pi}{n})$ . Next, observe that if the  $a_i$ 's were standard Gaussians then the following statements would hold. (a)  $\lambda_1$  is distributed  $\mathcal{N}(0,n)$ . (b)  $g_k$ 's and  $h_k$ 's are IID  $\mathcal{N}(0,1/2)$ ; therefore,  $\lambda_k^2 \stackrel{\text{iid}}{\sim} \frac{1}{2}\chi_2^2$  where  $\chi_2^2$  denotes a chi-squared random variable with two degrees of freedom. This leads to the following conclusion:

**Lemma 3.1.** Let the first row of a circulant **A** have entries drawn IID from standard Gaussians and let the MI be given as in (1) for  $d_i = d_i^*$  and for some average transmissivity  $\rho$ . Then,  $\mathbb{E}[\mathcal{I}]$  equals  $\mathbb{E}_{G \sim \mathcal{N}(0,1)} \log \left( \gamma_{\rho} G^2 + 1 \right) + 2 \sum_{k=2}^{\frac{n+1}{2}} \mathbb{E}_{X \sim \chi_2^2} \log \left( \gamma_{\rho} \frac{X \beta^{\frac{k-1}{(n-1)/2}}}{2n} + 1 \right)$ .

We conjecture that in the  $n \to \infty$  limit, the conclusion of Lemma 3.1 is universal over the distribution of the entries of  $\mathbf{a}^T$ , i.e., it holds for entries that have zero mean, unit variance, and bounded third moment. Based on this assumption, we posit that the expected mutual information  $\mathbb{E}[\mathcal{I}_p]$  for a random on-off circulant system with parameter 0 for the correlated scene model is given by:

$$\mathbb{E}_{G \sim \mathcal{N}(0,1)} \log \left( \frac{1}{n} \gamma_p \left( \sqrt{p(1-p)} \cdot G + p \sqrt{n} \right)^2 + 1 \right) + 2 \sum_{k=2}^{\frac{n+1}{2}} \mathbb{E}_{X \sim \chi_2^2} \log \left( \frac{1}{2n} \gamma_p p(1-p) X \beta^{\frac{k-1}{(n-1)/2}} + 1 \right).$$

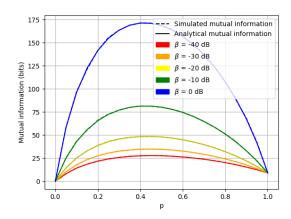
Remark 5. It is apparent from inspection of (3) that a lower  $\beta$  (i.e. a more correlated scene) implies a higher  $p^*$ . This effect can be observed in Figure 3, which also compares (3) against simulated data.

# 4. DISCUSSION AND FUTURE WORK

Our framework allows to rigorously analyze random on-off and spectrally-flat patterns for IID scenes and accurately characterize the optimal transmissivity of masks in a variety of different noise regimes. [7] raises the question of whether continuous-valued masks perform better than binary-valued ones; we plan to use our framework to find an answer in the future. In this work, we focused exclusively on 1D masks, which are relevant for example in de-blurring along one dimension [6]. We leave extensions to 2D masks to future work. However, we note that much of the analysis conducted here can be directly applied to study separable 2D apertures, i.e. ones that can be expressed as the outer product of two 1D apertures.

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**Fig. 3**: Analytical formula follows Eqn. (3). Simulated data are averages of 200 randomly generated apertures of size n=251 for various different values p. We set J/W=0 dB and  $\theta/W=30$  dB. Simulations match our analysis perfectly, providing support for the conjecture of (3).

#### A. PROOF SKETCHES

Proof sketch of Proposition 3.1: For convenience we use  $\lambda_i := \lambda_i(\mathbf{A})$ . We treat the DC-term of the spectrum, i.e.  $\lambda_1$ , separately from the rest. Note that  $\mathbf{A1} = (np)\mathbf{1}$ ; thus,  $\lambda_1 = np$ . Next, let us denote  $\mathcal{I}_{\sim 1}$  the MI in (1), excluding the term that involves  $\lambda_1$ . By concavity of  $\log$ ,  $\mathcal{I}_{\sim 1}$  is upper bounded by

$$(n-1)\log\left(\frac{\gamma}{(n-1)n^2}\sum_{i=2}^n|\lambda_i(\mathbf{A})|^2+1\right) \approx \frac{\gamma p(1-p)}{\ln(2)},$$
 (4)

where the bound is tight iff  $|\lambda_2|=|\lambda_3|=\ldots=|\lambda_n|$ ; (4) uses the fact that  $\sum_{i=2}^n |\lambda_i(\mathbf{A})|^2=\|\mathbf{A}\|_F^2-\lambda_1^2=n^2p(1-p)$  and  $n\approx n-1$  and  $n\log(\frac{\alpha}{n}+1)=\alpha/\ln(2)$  for large n. In particular, spectrally-flat patterns achieve the upper bound, which gives  $\mathcal{I}_{\mathrm{SF}}\approx\log(\frac{\gamma}{4}+1)+\frac{\gamma}{4\ln(2)}$ .

Proof sketch of Proposition 3.2: The proof leverages the following result of [21]. Consider a reverse circulant matrix  $\frac{1}{\sqrt{n}}\mathbf{B}$  with entries  $B_{ji} = b_{j+i-2 \mod n}$ , and  $(b_0, b_1, \ldots, b_n)$ . a sequence of IID random variables with mean zero, unit variance and bounded third moment. Then, the empirical spectral density (ESD) of  $\mathbf{B}$  converges to the limiting spectral distribution with density  $f_X(x) = |x|e^{-x^2}$ . In our setting, we are interested in the ESD of  $\mathbf{A}\mathbf{A}^T$  for  $\mathbf{A}$  that has entries  $\mathrm{Bern}(p)$ . To apply the result of [21], consider:  $\mathbf{A}' = (\mathbf{A} - p\mathbf{1}\mathbf{1}^T)/\sqrt{p(1-p)}$ . The entries of  $\mathbf{A}'$  have zero mean and unit variance. Moreover,  $\lambda_j(\mathbf{A}') = \lambda_j(\mathbf{A})/\sqrt{p(1-p)}$  for  $j=2,\ldots,n$ . It can be shown that  $|\lambda_j(\mathbf{A}')|^2 = \lambda_j^2(\mathbf{B})$  [21, Lem. 1]. Applying these to (1) gives  $\mathcal{I} = \sum_{i=1}^n \log\left(\frac{\theta_p(1-p)}{n(W+pJ)} \cdot \lambda_i^2\left(\frac{1}{\sqrt{n}}\mathbf{B}\right) + 1\right) \stackrel{n\to\infty}{\to} \widetilde{\mathcal{I}}_p$ , where the convergence result follows from a Taylor series expansion of  $\log(1+x)$ , the result of [21], and  $\int_{-\infty}^{\infty} x^2|x|e^{-x^2} = 1$ .

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