

A ROOT-MUSIC-LIKE DIRECTION FINDING METHOD FOR CYCLOSTATIONARY SIGNALS

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ABSTRACT

In this paper, we propose a new Root-MUSIC-like direction finding algorithm that exploits cyclostationarity in order to improve the direction-of-arrival estimation. The proposed cyclic method is signal selective, it allows to increase the resolution power and the noise robustness significantly, and it is also able to handle more sources than the number of sensors. Computer simulations are used to show the performance of the algorithm.

1. INTRODUCTION

The aim of this paper is the estimation of the direction-of-arrival (DOA) of impinging signals in the telecommunications systems area, where almost all signals exhibit the cyclostationarity property [4]. The cyclostationarity has been first introduced into array processing by Gardner [3]. We can find in the literature several algorithms (see [4]), that exploit cyclostationarity to improve the performances of the conventional methods. Instead of using the correlation matrix as in the conventional methods, these algorithms require the estimation of the cyclic correlation matrix that reflects the cyclostationarity of incoming signals, assuming they have baud rates and/or are carrier modulated signals as they would be in radar and radio communication applications. Recently, an extended cyclic MUSIC algorithm has been proposed in [6] that provides a rather good estimation performance. In [5] an extended Root-MUSIC (extension of the Root-MUSIC [1]) algorithm has been proposed in the non circular source case.

In this paper we propose an new extended cyclic direction finding method that allows to select desired signals and to ignore interferences, by exploiting the cyclostationarity property of the signals of interest. The proposed method is inspired from the extended Root-MUSIC method [5], and then is restricted to linear uniformly spaced arrays. But it has the distinct advantage over [6] in that it does not require a search over parameter space. Instead, our algorithm here

requires calculation of the roots of a polynomial, which is a simple process and has low computation cost.

2. DATA MODEL

In this paper we consider a uniform linear array of L antennas. Suppose K electromagnetic waves impinging on the array from angular directions θ_k , $k = 1, \dots, K$. The incident waves are assumed to be plane waves, as generated from far-field point sources. Furthermore, the signals are assumed to be narrow band. In our study, we assume that K_α sources emit cyclostationary signals with cycle frequency α (with $K_\alpha \leq K$). In the following, we consider that $\mathbf{s}(t)$ contains only the K_α signals that exhibit cycle frequency α , and all of the remaining $K - K_\alpha$ signals (that have not cycle frequency α) and any noise are lumped into a vector $\mathbf{i}(t)$. Using this assumption, the signal received by the array from the emitting narrowband sources can be written as :

$$\mathbf{z}(t) = \mathbf{A}\mathbf{s}(t) + \mathbf{i}(t) \quad (1)$$

where the vector $\mathbf{s}(t) = [s_1(t), \dots, s_{K_\alpha}(t)]^T$ contains the temporal signals that have cycle frequency α , the vector $\mathbf{i}(t)$ represents interfering sources and noise. The matrix $\mathbf{A} = [\mathbf{a}(\theta_1), \dots, \mathbf{a}(\theta_{K_\alpha})]$ contains the steering vectors of the impinging signals of interest (SOI). We assume that the received signals are sampled at N distinct times t_n , $n = 1, 2, \dots, N$.

The cyclic autocorrelation matrix and the cyclic conjugate autocorrelation matrix at cycle frequency α for some lag parameter τ are then nonzero and can be estimated by :

$$\mathbf{R}_{\mathbf{z}\mathbf{z}}^\alpha(\tau) = \frac{1}{N} \sum_{n=1}^N \mathbf{z}(t_n + \tau/2) \mathbf{z}^H(t_n - \tau/2) e^{-j2\pi\alpha t_n} \quad (2)$$

and

$$\mathbf{R}_{\mathbf{z}\mathbf{z}^*}^\alpha(\tau) = \frac{1}{N} \sum_{n=1}^N \mathbf{z}(t_n + \tau/2) \mathbf{z}^T(t_n - \tau/2) e^{-j2\pi\alpha t_n} \quad (3)$$

We form the following extended-data vector :

$$\mathbf{z}_{CE}(t) = \begin{bmatrix} \mathbf{z}(t) \\ \mathbf{z}^*(t) \end{bmatrix} \quad (4)$$

The cyclic correlation matrix for this extended data model can be estimated as :

$$\mathbf{R}_{CE}^\alpha(\tau) = \frac{1}{N} \sum_{n=1}^N \mathbf{I}_{2L}^\alpha(t_n) \mathbf{z}_{CE}(t_n + \tau/2) \mathbf{z}_{CE}^H(t_n - \tau/2) \quad (5)$$

where the time dependent matrix $\mathbf{I}_{2L}^\alpha(t)$ is defined by :

$$\mathbf{I}_{2L}^\alpha(t) = \begin{bmatrix} \mathbf{I}_L e^{-j2\pi\alpha t} & \mathbf{0} \\ \mathbf{0} & \mathbf{I}_L e^{+j2\pi\alpha t} \end{bmatrix} \quad (6)$$

and \mathbf{I}_L is the L -dimensional identity matrix. This extended cyclic correlation matrix can be developed as :

$$\mathbf{R}_{CE}^\alpha(\tau) = \begin{bmatrix} \mathbf{R}_{zz}^\alpha(\tau) & \mathbf{R}_{zz^*}^\alpha(\tau) \\ \mathbf{R}_{zz^*}^{\alpha*}(\tau) & \mathbf{R}_{zz}^{\alpha*}(\tau) \end{bmatrix} \quad (7)$$

where the matrices $\mathbf{R}_{zz}^\alpha(\tau)$ and $\mathbf{R}_{zz^*}^\alpha(\tau)$ are estimated by (2) and (3) respectively.

By choosing the cycle frequency parameter α in the estimation of the extended correlation matrix to be the cycle frequency of the K_α signals of interest (SOI), the contribution to the cyclic correlation matrix from the other $K - K_\alpha$ signals (assumed not to have the same cycle frequency) and from any noise converges to zero as the integration time used in the estimate tends to infinity.

3. DOA ESTIMATION

By computing the SVD of $\mathbf{R}_{CE}^\alpha(\tau)$ similarly to the Cyclic MUSIC algorithm, a left signal subspace can be defined by the K'_α left singular vectors associated with the K'_α nonzero singular values. These singular vectors form the column vectors of the matrix \mathbf{U}_s . In the same way a left null-space is spanned by the remaining $2L - K'_\alpha$ singular vectors associated with the zero singular values of $\mathbf{R}_{CE}^\alpha(\tau)$, and these singular vectors are the column vectors of the matrix \mathbf{U}_n . Note that in the practice, there are no zero singular values but only small singular values, and the dimension on the signal subspace can be estimated by the MDL criterion [2]. Some cyclostationary signals have a rank two in the signal subspace spanned by column vectors of the matrix \mathbf{U}_s and others have only a rank one, so that the dimension of the signal subspace is equal to K'_α with $K_\alpha \leq K'_\alpha \leq 2K_\alpha$ (see [6] for more details).

As in [6], it can be defined an extended steering vector corresponding to this data model as

$$\mathbf{b}(\theta, \mathbf{k}) = \begin{bmatrix} \mathbf{a}(\theta) & \mathbf{0} \\ \mathbf{0} & \mathbf{a}^*(\theta) \end{bmatrix} \mathbf{k} \quad (8)$$

where \mathbf{k} is a (2×1) vector.

According to the subspace based methods principle and by using this extended steering vector, the DOA of the SOI are given by the minima of the following function :

$$\bar{P}(\theta, \mathbf{k}) = \|\mathbf{U}_n^H \mathbf{b}(\theta, \mathbf{k})\|^2 = \mathbf{k}^H \mathbf{M} \mathbf{k} \quad (9)$$

where \mathbf{M} is a (2×2) matrix

$$\mathbf{M} = \begin{bmatrix} \mathbf{a}^H(\theta) \mathbf{U}_{n1} \mathbf{U}_{n1}^H \mathbf{a}(\theta) & \mathbf{a}^H(\theta) \mathbf{U}_{n1} \mathbf{U}_{n2}^H \mathbf{a}^*(\theta) \\ \mathbf{a}^T(\theta) \mathbf{U}_{n2} \mathbf{U}_{n1}^H \mathbf{a}(\theta) & \mathbf{a}^T(\theta) \mathbf{U}_{n2} \mathbf{U}_{n2}^H \mathbf{a}^*(\theta) \end{bmatrix} \quad (10)$$

and \mathbf{U}_{n1} and \mathbf{U}_{n2} are two submatrices of the same dimension

$$\mathbf{U}_n = \begin{bmatrix} \mathbf{U}_{n1} \\ \mathbf{U}_{n2} \end{bmatrix} \quad (11)$$

It can be shown [6] that $\mathbf{U}_{n2}^* \mathbf{U}_{n2}^T = \mathbf{U}_{n1} \mathbf{U}_{n1}^H$. So, the two diagonal elements of the matrix \mathbf{M} are equal. Note also that the two non diagonal elements form a complex conjugate pair.

The minimum of the quadratic form in (9) over θ and \mathbf{k} is given by the smallest eigenvalue of the matrix \mathbf{M} . This eigenvalue is always nonnegative since the quadratic form is nonnegative. When θ is a true DOA, the smallest eigenvalue of \mathbf{M} is equal to zero, and then the determinant of the matrix \mathbf{M} equals zero too.

Let's now define the complex variable z ,

$$z = e^{j \frac{2\pi\delta}{\lambda} \sin(\theta)} \quad (12)$$

where δ denotes the distance between two adjacent antennas and λ the wavelength of impinging SOI. Then $\mathbf{a}(\theta)$ can be written as

$$\mathbf{a}(z) = [1, z, z^2, \dots, z^{L-1}]^T \quad (13)$$

and the matrix \mathbf{M} is a function of z . We estimate the DOAs by finding the values of z such that

$$\det\{\mathbf{M}\} = 0 \quad (14)$$

The left side of (14) is a polynomial of z . The DOA estimation problem is then transformed into a polynomial rooting problem that can be solved using computationally efficient root-solving algorithms.

The polynomial of z can take the following form:

$$\det\{\mathbf{M}\} = m_{11}^2 - m_{12}m_{21} \quad (15)$$

where

$$\begin{cases} m_{11} &= \mathbf{a}^T(1/z) \mathbf{U}_{n1} \mathbf{U}_{n1}^H \mathbf{a}(z) \\ m_{12} &= \mathbf{a}^T(1/z) \mathbf{U}_{n1} \mathbf{U}_{n2}^H \mathbf{a}(1/z) \\ m_{21} &= \mathbf{a}^T(z) \mathbf{U}_{n2} \mathbf{U}_{n1}^H \mathbf{a}(z) \end{cases} \quad (16)$$

Therefore m_{11} is a polynomial in z whose l^{th} coefficient is given by the sum of the elements of the l^{th} diagonal of

$\mathbf{U}_{n1}\mathbf{U}_{n1}^H$, where $l = -L + 1$ indicates the lowest diagonal and $l = L - 1$ indicates the highest diagonal. Let $\mathbf{c} = [c_1, \dots, c_{2L-1}]^T$ be the column vector of the coefficients of the polynomial m_{11} , we have

$$m_{11} = [z^{-L+1}, \dots, z^{-1}, 1, z, \dots, z^{L-1}] \mathbf{c} = \sum_{p=1}^{2L-1} c_p z^{p-L} \quad (17)$$

with

$$c_p = \sum_{i=\max[1, L-p+1]}^{\min[L, 2L-p]} [\mathbf{U}_{n1}\mathbf{U}_{n1}^H]_{i, p+i-L} \quad (18)$$

Then we can write that

$$m_{11}^2 = [z^{-L+1}, \dots, z^{L-1}] \mathbf{c} \mathbf{c}^T [z^{-L+1}, \dots, z^{L-1}]^T$$

Hence the coefficients of the polynomial m_{11}^2 equal the sum of the antidiagonal elements of the matrix $\mathbf{c} \mathbf{c}^T$. Let $\mathbf{s} = [s_1, \dots, s_{4L-3}]^T$ be the vector containing these $4L - 3$ coefficients. For $p = 1, \dots, 4L - 3$ we have

$$s_p = \sum_{i=\max[1, p-2L+2]}^{\min[2L-1, p]} [\mathbf{c} \mathbf{c}^T]_{i, p-i+1} \quad (19)$$

We obtain

$$m_{11}^2 = \sum_{p=1}^{4L-3} s_p z^{p-(2L-1)} \quad (20)$$

The matrix $\mathbf{U}_{n1}\mathbf{U}_{n1}^H$ being a hermitian matrix, the elements of the vector \mathbf{c} have the symmetry property $c_i = c_{2L-i}^*$. Since $\mathbf{c} \mathbf{c}^T$ is a symmetrical matrix, the coefficients of the polynomial m_{11}^2 keep the same property of symmetry $s_p = s_{4L-2-p}^*$.

In the same way, let \mathbf{u} be the column vector containing the sum of the $2L - 1$ antidiagonal elements of the matrix $\mathbf{U}_{n1}\mathbf{U}_{n2}^H$ such that for $p = 1, \dots, 2L - 1$

$$u_p = \sum_{i=\max[1, p-L+1]}^{\min[L, p]} [\mathbf{U}_{n1}\mathbf{U}_{n2}^H]_{i, p-i+1} \quad (21)$$

Then, we can show that

$$m_{12} = [1, z^{-1}, \dots, z^{-(2L-2)}] \mathbf{u} \quad (22)$$

$$m_{21} = [1, z, \dots, z^{2L-2}] \mathbf{u}^* \quad (23)$$

and

$$m_{12}m_{21} = [1, \dots, z^{-2L+2}] \mathbf{u} \mathbf{u}^H [1, \dots, z^{2L-2}]^T \quad (24)$$

Let \mathbf{r} be the column vector whose elements are the sum of the diagonal elements of the matrix $\mathbf{u} \mathbf{u}^H$. For $p = 1, \dots, 4L - 3$ the coefficients are

$$r_p = \sum_{i=\max[1, 2L-p]}^{\min[2L-1, 4L-p-2]} [\mathbf{u} \mathbf{u}^H]_{i, p+i-(2L-1)} \quad (25)$$

Hence

$$m_{12}m_{21} = \sum_{p=1}^{4L-3} r_p z^{p-(2L-1)} \quad (26)$$

The matrix $\mathbf{u} \mathbf{u}^H$ being a hermitian matrix, the coefficients of the polynomial $m_{12}m_{21}$ also have the property of symmetry $r_p = r_{4L-2-p}^*$.

Equation (14) can now be written:

$$\det\{\mathbf{M}\} = \sum_{p=1}^{4L-3} (s_p - r_p) z^{p-(2L-1)} = 0 \quad (27)$$

The roots of the polynomial $\det\{\mathbf{M}\}$ can be computed using any polynomial rooting algorithm. The DOA estimates are obtained using (12):

$$\theta_k = \arcsin\left(\frac{\lambda}{2\pi\delta} \arg(z_n)\right) \quad (28)$$

where z_n represents one of the K_α roots selected for DOA estimation. Due to the symmetry property of the polynomial coefficients, roots appear in reciprocal conjugate pairs z_i and $1/z_i^*$. In each pair one root is inside the unit circle while the other is outside the unit circle (the two roots coincide if they are on the unit circle). Either one of the two can be used for DOA estimation, since they have the same angle in the complex plane. We can decide to use the roots inside the unit circle. We then select the K_α roots that are nearest to the unit circle as being the roots corresponding to the DOA estimates.

Note that the degree of the polynomial $\det\{\mathbf{M}\}$ is $4L - 4$ ($4L - 3$ coefficients). Hence the number of roots is $4L - 4$, and since roots appear in reciprocal pairs, the proposed procedure allows to determine until $2(L - 1)$ possible DOA. This has to be emphasized since the number of DOA estimates can be larger than the number of sensors. This characteristic is due to the used data model here.

4. SIMULATION RESULTS

In this section we present some simulation results that illustrate the performance of the proposed algorithm. We also compare the simulation results of the proposed procedure with those of the classical Root-MUSIC algorithm.

We consider here a linear uniformly spaced array with 6 sensors spaced by a half wavelength of the incoming signals. Incoming BPSK cyclostationary signals are generated with noise, and the signal to noise ratio (SNR) is 0 dB for each signal. The bit rate of the BPSK signals of interest (SOI) is 4 Mb/s. Other signals are considered as interferers, and which are BPSK modulated signals with a 3.2 Mb/s bit rate. In order to choose correctly the parameters α and τ , we have estimated the magnitude of cyclic correlation function (Figure 1) for a 4 Mb/s BPSK modulated

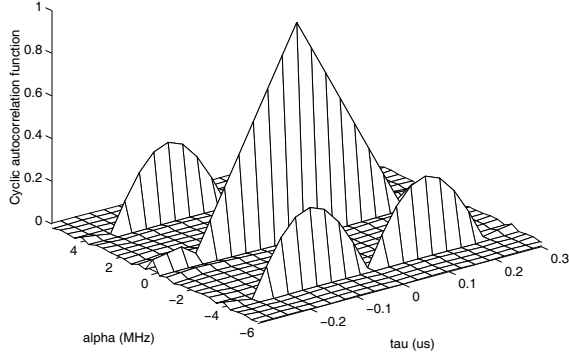


Fig. 1. Magnitude of the BPSK cyclic autocorrelation function versus α and τ .

signals sampled with the frequency 32 MHz during $25\mu\text{s}$. It can be noted that the magnitude of the cyclic autocorrelation function and that of the conjugate cyclic autocorrelation function are equal for a BPSK signal. According to this result, the proposed method and the Cyclic MUSIC algorithm are simulated with $\alpha = 4 \text{ MHz}$ and $\tau = 0.125\mu\text{s}$. In the next simulations, the averaging time is equal to $25\mu\text{s}$ and the sample frequency is 32 MHz . The contribution of both the interferer signals and that of the noise are theoretically zero in the two cyclic correlation matrices.

The performance of the estimators in each of the simulations below is obtained from 1000 Monte-Carlo simulations, by calculating the mean and the standard deviation of DOA estimates. Table 1 shows simulation results when two BPSK SOI arrive from -4° and 4° , and one interferer BPSK source from 16° DOA.

		SOI #1	SOI #2	Interf.
	True DOAs ($^\circ$)	-4	4	16
Proposed method	mean	-4.008	3.992	-
	std deviation	0.257	0.187	-
Root method	mean	-3.871	3.908	15.964
	std deviation	0.572	0.991	0.385

Table 1. Means and standard deviations for both methods

The proposed cyclic method allows to perfectly select the two SOI, and ignores the interferer signal. The proposed cyclic algorithm performs better than the classical Root-MUSIC thanks to the exploitation of the both cyclic correlation matrices ; more information about sources is used and the observation dimension space (i.e. the size of the extended covariance matrix $\mathbf{R}_{CE}^\alpha(\tau)$) is doubled.

Table 2 provides simulation results for only the proposed procedure when 7 SOI and 7 interferer BPSK sources impinge on the 6-sensors array. DOA of SOI are -70° ,

	True DOAs ($^\circ$)	mean	std deviation
SOI #1	-70	-69.649	1.012
SOI #2	-50	-49.986	0.512
SOI #3	-30	-30.005	0.442
SOI #4	-10	-10.005	0.289
SOI #5	20	19.989	0.623
SOI #6	40	40.017	0.542
SOI #7	60	59.945	0.734

Table 2. Mean and standard deviation for proposed method with 7 SOI and 7 interferer signals

-50° , -30° , -10° , 20° , 40° and 60° . DOA of interferer signals are -35° , -20° , 0° , 15° , 25° , 30° and 45° . The method always ignores interferer signals and gives rather accurate estimations of the SOI DOA. These last results show that the proposed method is signal selective and is able to handle more sources than the number of sensors.

5. CONCLUSION

We have described a signal selective procedure for DOA estimation. By assuming that incoming signals are BPSK modulated signals, the algorithm uses the cyclostationary property of the signals to improve the estimations performance. The proposed method is able to handle more sources than the number of sensors. Moreover by using a polynomial rooting technique, the proposed algorithm does not require an explicit search procedure, and hence considerably reduces the computational requirements.

6. REFERENCES

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